average value. The average value depends on the averaging time employed in analysing the meteorological data and this averaging time varies from a few seconds to several minutes. The magnitude of fluctuating component of the wind speed which is called gust, depends on the averaging time. In general, smaller the averaging interval, greater is the magnitude of the gust speed.

- 5.2 Basic Wind Speed Figure 1 gives basic wind speed map of India, as applicable to 10 m height above mean ground level for different zones of the country. Basic wind speed is based on peak gust velocity averaged over a short time interval of about 3 seconds and corresponds to mean heights above ground level in an open terrain (Category 2). Basic wind speeds presented in Fig. 1 have been worked out for a 50 year return period. Basic wind speed for some important cities/towns is also given in Appendix A.
- 5.3 Design Wind Speed (V_z) The basic wind speed (V_b) for any site shall be obtained from Fig. 1 and shall be modified to include the following effects to get design wind velocity at any height (V_z) for the chosen structure:
 - a) Risk level;
 - b) Terrain roughness, height and size of structure; and
 - c) Local topography.

It can be mathematically expressed as follows:

$$V_z = V_b k_1 k_2 k_3$$

where

- V_z = design wind speed at any height z in m/s;
- k₁ = probability factor (risk coefficient) (see 5.3.1);
- k_2 = terrain, height and structure size factor (see 5.3.2); and
- $k_3 = \text{topography factor (see 5.3.3)}.$

Note - Design wind speep up to 10 m height from mean ground level shall be considered constant.

- 5.3.1 Risk Coefficient (k_1 Factor) Figure 1 gives basic wind speeds for terrain Category 2 as applicable at 10 m above ground level based on 50 years mean return period. The suggested life period to be assumed in design and the corresponding k_1 factors for different class of structures for the purpose of design is given in Table 1. In the design of all buildings and structures, a regional basic wind speed having a mean return period of 50 years shall be used except as specified in the note of Table 1.
- 5.3.2 Terrain, Height and Structure Size Factor (k2 Factor)
- 5.3.2.1 Terrain Selection of terrain categories shall be made with due regard to the effect

of obstructions which constitute the ground surface roughness. The terrain category used in the design of a structure may vary depending on the direction of wind under consideration. Wherever sufficient meteorological information is available about the nature of wind direction, the orientation of any building or structure may be suitably planned.

Terrain in which a specific structure stands shall be assessed as being one of the following terrain categories:

a) Category 1 — Exposed open terrain with few or no obstructions and in which the average height of any object surrounding the structure is less than 1.5 m.

Note — This category includes open sea-coasts and flat treeless plains.

- b) Category 2 Open terrain with well scattered obstructions having heights generally between 1.5 to 10 m.
 - Note This is the criterion for measurement of regional basic wind speeds and includes airfields, open parklands and undeveloped sparsely built-up outskirts of towns and suburbs. Open land adjacent to sea coast may also be classified as Category 2 due to roughness of large sea waves at high winds.
- c) Category 3 Terrain with numerous closely spaced obstructions having the size of building-structures up to 10 m in height with or without a few isolated tall structures.

Note 1 — This category includes well wooded areas, and shrubs, towns and industrial areas full or partially developed.

Note 2—It is likely that the next higher category than this will not exist in most design situations and that selection of a more severe category will be deliberate.

- Note 3 Particular attention must be given to performance of obstructions in areas affected by fully developed tropical cyclones. Vegetation which is likely to be blown down or defoliated cannot be relied upon to maintain Category 3 conditions. Where such situation may exist, either an intermediate category with velocity multipliers midway between the values for Category 2 and 3 given in Table 2, or Category 2 should be selected having due regard to local conditions.
- d) Category 4 Terrain with numerous large high closely spaced obstructions.

Note — This category includes large city centres, generally with obstructions above 25 m and well developed industrial complexes.

5.3.2.2 Variation of wind speed with height for different sizes of structures in different terrains (k_2 factor) — Table 2 gives multiplying factors (k_2) by which the basic wind speed given in Fig. 1 shall be multiplied to obtain the wind speed at different heights, in each terrain category for different sizes of buildings/structures.

The buildings/structures are classified into the following three different classes depending upon their size:

Class A — Structures and/or their components such as cladding, glazing, roofing, etc, having maximum dimension (greatest horizontal or vertical dimension) less than 20 m.

Class B - Structures and/or their com-

ponents such as cladding, glazing, roofing, etc, having maximum dimension (greatest horizontal or vertical dimension) between 20 and 50 m.

Class C — Structures and/or their components such as cladding, glazing, roofing, etc, having maximum dimension (greatest horizontal or vertical dimension) greater than 50 m.

TABLE 1 RISK COEFFICIENTS FOR DIFFERENT CLASSES OF STRUCTURES IN DIFFERENT WIND SPEED ZONES

(Clause 5.3.1)

| CLASS OF STRUCTURE | MEAN PROBABLE DESIGN LIFE OF | k ₁ Factor for Basic Wind Speed (m/s) of | | | | | |
|--|---------------------------------|---|------|------|------|-------|------|
| | STRUCTURE IN YZARS | 33 | 39 | 44 | 47 | 47 50 | 55 |
| All general buildings and structures | 50 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Temporary sheds, structures such as those used during construction operations (for example, formwork and falsework), structures during construction stages and boundary wails | 5 | 0.82 | 0.76 | 0.73 | 0.41 | 0.70 | 0.57 |
| Buildings and structures presenting a low degree of hazard to life and property in the event of failure, such as isolated towers in wooded areas, farm buildings other than residential buildings | 25 | 0.94 | 0.92 | 0.91 | 0.90 | 0.90 | 0.89 |
| Important buildings and structures such as hospitals communication buildings / towers, power plant structures | 100 | 1.02 | 1.06 | 1.07 | 1.07 | 1.08 | 1.08 |

Note — The factor k_1 is based on statistical concepts which take account of the degree of reliability required and period of time in years during which these will be exposure to wind, that is, life of the structure. Whatever wind speed is adopted for design purposes, there is always a probability (however small) that it may be exceeded in a storm of exceptional violence; the greater the period of years over which these will be exposure to the wind, the greater is the probability. Higher return periods ranging from 100 to 1 000 years (implying lower risk level) in association with greater periods of exposure may have to be selected for exceptionally important structures, such as, nuclear power reactors and satellite communication towers. Equation given below may be used in such cases to estimate k_1 factors for different periods of exposure and chosen probability of exceedance (risk level). The probability level of 0.63 is normally considered sufficient for design of buildings and structures against wind effects and the values of k_1 corresponding to this risk level are given above.

$$k_{1} = \frac{X_{N, P}}{X_{50, 0.63}} = \frac{A - B \left[ln \left\{ -\frac{1}{N} ln \left(1 - P_{N} \right) \right\} \right]}{A + 4B}$$

where

N = mean probable design life of structure in years;

 P_N = risk level in N consecutive years (probability that the design wind speed is exceeded at least once in N successive years), nominal value = 0.63;

 $X_{N,P}$ = extreme wind speed for given values of N and P_N ; and

 $X_{50,\ 0.63} = \text{ extreme wind speed for } N = 50 \text{ years and } P_N = 0.63.$

A and B are coefficients having the following values for different basic wind speed zones:

| Zone | A | В | | |
|--------|------|------|--|--|
| 33 m/s | 33.2 | 9.2 | | |
| 39 m/s | 84.0 | 14.0 | | |
| 4+ m/s | 83.0 | 18.0 | | |
| 47 m/s | 0.88 | 20.5 | | |
| 50 m/s | 80.3 | 22.8 | | |
| 55 m/s | 90.8 | 27.3 | | |

TABLE 2 k, FACTORS TO OBTAIN DESIGN WIND SPEED VARIATION WITH HEIGHT IN DIFFERENT TERRAINS FOR DIFFERENT CLASSES OF BUILDINGS/STRUCTURES

(Clause 5.3.2.2)

| Неіснт | TERR | AIN CATE CLASS | | | CLASS | GORY 2 | TERRAIN CATEGORY 3 CLASS | | TERRAIN CATEGORY 4 CLASS | | | |
|---------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| m | $a^{}$ | B | \overline{c} | | В | \overline{c} | \overline{A} | B | \overline{c} | 7 | | \overline{c} |
| (I) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) |
| 10 15 20 30 50 | 1.05 1.09 1.12 1.15 1.20 | 1.03 1.07 1.10 1.13 1.18 | 0.99 1.03 1.06 1.09 1.14 | 1·00 1·05 1·07 1·12 1·17 | 0.98 1.02 1.05 1.10 1.15 | 0.93 0.97 1.00 1.04 1.10 | 0·91 0·97 1·01 1·06 1·12 | 0.88 0.94 0.98 1.03 1.05 | 0.82 0.87 0.91 0.96 1.02 | 0.80 0.80 0.80 0.97 1.10 | 0·76 0·76 0·76 0·93 1·05 | 0·67 0·67 0·67 0·83 0·95 |
| 106 150 200 250 306 | 1·26 1·30 1·32 1·34 1·35 | 1·24 1·28 1·30 1·32 1·34 | 1·26 1·26 1·28 1·30 | 1·24 1·28 1·30 1·32 1·34 | 1·22 1·25 1·28 1·31 1·32 | 1·17 1·21 1·24 1·26 1·28 | 1·20 1·24 1·27 1·29 1·31 | 1·17 1·21 1·24 1·26 1·28 | 1·16 1·15 1·18 1·20 1·22 | 1·26 1·24 1·27 1·28 1·30 | 1·15 1·26 1·22 1·24 1·26 | 1.05 1.10 1.13 1.16 1.17 |
| 350 400 450 500 | 1·37 1·38 1·39 1·40 | 1·35 1·36 1·37 1·38 | 1·31 1·32 1·33 1·34 | 1·36 1·37 1·38 1·39 | 1·34 1·35 1·36 1·37 | 1·29 1·31 1·32 | 1·32 1·34 1·35 I·36 | 1·36 1·31 1·32 1·33 | 1·24 1·25 1·26 1·28 | 1·31 1·32 1·33 1·34 | 1·27 1·28 1·29 1·30 | 1·19 1·20 1·21 1·22 |

NOTE 1 - See 5.3.2.2 for definitions of Class A, Class B and Class C structures.

Note 2 — Intermediate values may be obtained by linear interpolation, if desired. It is permissible to assume constant wind speed between 2 heights for simplicity.

5.3.2.3 Terrain categories in relation to the direction of wind — The terrain category used in the design of a structure may vary depending on the direction of wind under consideration. Where sufficient meteorological information is available, the basic wind speed may be varied for specific wind direction.

5.3.2.4 Changes in terrain categories — The velocity profile for a given terrain category does not develop to full height immediately with the commencement of that terrain category but develop gradually to height (h_x) which increases with the fetch or upwind distance (x).

- a) Fetch and developed height relationship The relation between the developed height (h_x) and the fetch (x) for wind-flow over each of the four terrain categories may be taken as given in Table 3.
- b) For structures of heights greater than the developed height (h_x) in Table 3, the velocity profile may be determined in accordance with the following:
 - i) The less or least rough terrain, or
 - ii) The method described in Appendix B.

5.3.3 Topography (k_3 Factor) — The basic wind speed V_b given in Fig. 1 takes account of the general level of site above sea level. This does not allow for local topographic features such as hills, valleys, cliffs, escarpments, or ridges which can significantly affect wind speed in their vicinity. The effect of topography is to accelerate wind near the summits of hills or crests of cliffs, escarpments or ridges and decelerate the wind in valleys or near the foot of cliffs, steep escarpments, or ridges.

TABLE 3 FETCH AND DEVELOPED HEIGHT RELATIONSHIP

(Clause 5.3.2.4)

| FETCH (x) | DEVELOPED HEIGHT, hx IN METRES | | | | | | |
|-----------|--------------------------------|-----------------------|-----------------------|-----------------------|--|--|--|
| ž.iii | Terrain Category 1 | Terrain Category 2 | Terrain Category 3 | Terrain Category 4 | | | |
| (1) | (2) | (3) | (4) | (5) | | | |
| 0.5 | 12 | 20 | 35 | 60 | | | |
| 0.2 | 20 | 30 | 35 | 95 | | | |
| 1 | 25 | 45 | 80 | 130 | | | |
| 2 | 35 | 65 | 110 | 190 | | | |
| 5 | 60 | 100 | 170 | 300 | | | |
| 10 | 03 | 140 | 25C | 450 | | | |
| 20 | 120 | 200 | 350 | 500 | | | |
| 50 | 180 | 300 | 400 | 500 | | | |

5.3.3.1 The effect of topography will be significant at a site when the upwind slope (θ) is greater than about 3°, and below that, the value of k_3 may be taken to be equal to 1·0. The value of k_3 is confined in the range of 1·0 to 1·36 for slopes greater than 3°. A method of evaluating the value of k_3 for values greater than 1·0 is given in Appendix G. It may be noted that the value of k_3 varies with height above ground level, at a maximum near the ground, and reducing to 1·0 at higher levels.

5.4 Design Wind Pressure — The design wind pressure at any height above mean ground level shall be obtained by the following relationship between wind pressure and wind velocity:

 $p_z = 0.6 \, \Gamma_z^z$

where

p_z = design wind pressure in N/m² at height z, and

 $V_z = \text{design wind velocity in m/s at height } z$.

Note — The coefficient 0.6 (in SI units) in the above formula depends on a number of factors and mainly on the atmospheric pressure and air temperature. The value chosen corresponds to the average appropriate Indian atmospheric conditions.

5.5 Off Shore Wind Velocity — Cyclonic storms form far away from the sea coast and gradually reduce in speed as they approach the sea coast. Cyclonic storms generally extend up to about 60 kilometres inland after striking the coast. Their effect on land is already reflected in basic wind speeds specified in Fig. 1. The influence of wind speed off the coast up to a distance of about 200 kilometres may be taken as 1.15 times the value on the nearest coast in the absence of any definite wind data.

6. WIND PRESSURES AND FORCES ON BUILDINGS/STRUCTURES

- 6.1 General The wind load on a building shall be calculated for:
 - a) The building as a whole,
 - Individual structural elements as roofs and walls, and
 - Individual cladding units including glazing and their fixings.
- 6.2 Pressure Coefficients The pressure coefficients are always given for a particular surface or part of the surface of a building. The wind load acting normal to a surface is obtained by multiplying the area of that surface or its appropriate portion by the pressure coefficient (C_p) and the design wind pressure at the height of the surface from the ground. The average values of these pressure coefficients for some building shapes are given in 6.2.2 and 6.2.3.

Average values of pressure coefficients are given for critical wind directions in one or more quadrants. In order to determine the maximum wind load on the building, the total load should be calculated for each of the critical directions shown from all quadrants. Where considerable variation of pressure occurs over a surface, it has been subdivided and mean pressure coefficients given for each of its several parts.

In addition, areas of high local suction (negative pressure concentration) frequently occurring near the edges of walls and roofs are separately shown. Coefficients for the local effects should only be used for calculation of forces on these local areas affecting roof sheeting, glass panels, individual cladding units including their fixtures. They should not be used for calculating force on entire structural elements such as roof, walls or structure as a whole.

Note ! — The pressure coefficients given in different tables have been obtained mainly from measurements on models in winds tunnels, and the great majority for data available has been obtained in conditions of relatively smooth flow. Where sufficient field data exists as in the case of rectangular buildings, values have been obtained to allow for turbulent flow.

Note 2 — In recent years, wall glazing and cladding design has been a source of major concern. Although of less consequence than the collapse of main structures, damage to glass can be hazardous and cause considerable financial losses.

NOTE 3 — For pressure coefficients for structures not covered here, reference may be made to specialist literature on the subject or advise may be sought from specialists in the subject.

6.2.1 Wind Load on Individual Members — When calculating the wind load on individual structural elements such as roofs and walls, and individual cladding units and their fittings, it is essential to take account of the pressure difference between opposite faces of such elements or units. For clad structures, it is, therefore, necessary to know the internal pressure as well as the external pressure. Then the wind load. F, acting in a direction normal to the individual structural element or cladding unit is:

$$F = (C_{pe} - C_{pi}) A p_d$$

where

Cpe = external pressure coefficient,

Cpt = internal pressure coefficient,

A = surface area of structural element or cladding unit, and

pd = design wind pressure.

Note ! — If the surface design pressure varies with height, the surface areas of the structural element may be sub-divided so that the specified pressures are taken over appropriate areas.

Note 2 — Positive wind load indicates the force acting towards the structural element and negative away from it.

6.2.2 External Pressure Coefficients

6.2.2.1 Walls — The average external pressure coefficient for the walls of clad buildings of rectangular plan shall be as given in Table 4. In addition, local pressure concentration coefficients are also given.

6.2.2.2 Pitched roofs of rectangular clad buildings — The average external pressure coefficients and pressure concentration coefficients for pitched roofs of rectangular clad building shall be as given in Table 5. Where no pressure concentration coefficients are given, the average coefficients shall apply. The pressure coefficients on the underside of any overhanging roof shall be taken in accordance with 6.2.2.7.

Note 1 — The pressure concentration shall be assumed to act outward (suction pressure) at the ridges, eaves, cornices and 90 degree corners of roofs (see 6.2.2.7).

Note 2 — The pressure concentration shall not be included with the net external pressure when computing overall loads.