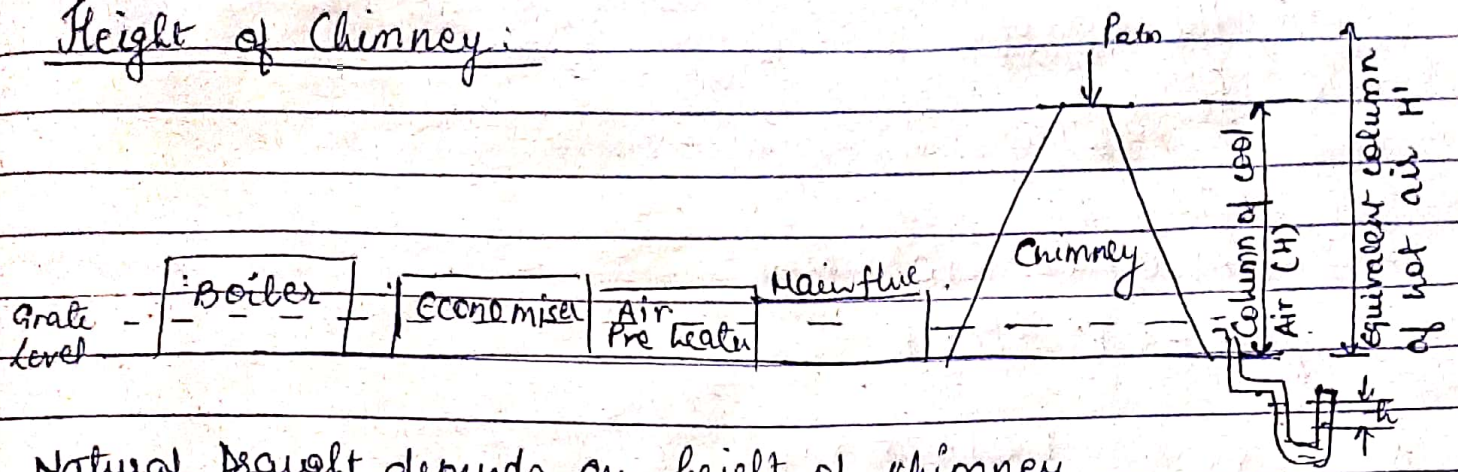


Height of Chimney:



Natural Draught depends on height of chimney.

Let,

m_a = Mass of air supplied in kg/kg of fuel

m_{a+1} = Mass of chimney gases (kg/kg of fuel)

T_a = absolute temperature of atmosphere

T_g = average absolute temperature of chimney gases

P_a = Atmospheric pressure (N/m^2)

H = Height of chimney (m)

ρ_a = Mass density of air outside chimney

ρ_g' = Avg. Mass density of hot gases

\therefore Static Draught : Difference of pressure causing the flow of gases. Its value is small & generally measured by a water manometer

$$\Delta P < \pm 2 \text{ mm of } H_2O$$

Static Draught = Pressure at grate on open side (P_2)
- Pressure at chimney side (P_1)

We have,

$$P_1 = P_a + \rho_g' \cdot g \cdot H$$

$$P_2 = P_a + \rho_a \cdot g \cdot H$$

$\rho_g' \cdot g \cdot H$ = Pressure exerted by column of hot gases of height 'H' m

$\rho_a \cdot g \cdot H$ = Pressure due to column of cold air outside chimney of height 'H' m

So,

$$\Delta P = P_2 - P_1 = (\rho_a - \rho_g') \cdot g \cdot H$$

(A)

specific volume of air at N.T.P.

$$v_0 = \frac{RT_0}{P_0}$$

$$= \frac{0.287 \text{ kJ/kg}\cdot\text{K} \times 273 \text{ K}}{101.325 \text{ kPa}}$$

$$= 0.7732 \text{ m}^3/\text{kg}$$

∴ The volume of fuel gas is negligible as compared to volume of air supplied per kg of fuel
∴ Volume of flue gases can be taken equal to volume of air

From Charles Law: ($V \propto T$)

$$\frac{v_a}{T_a} = \frac{v_0}{T_0} = \frac{m_a v_0}{T_0}$$

$$v_a = \frac{m_a \times 0.7732}{273} T_a$$

So,

$$\rho_a = \frac{m_a}{v_a} = \frac{273}{0.7732} \times \frac{1}{T_a} = \frac{353}{T_a}$$

~~Similarly volume of~~

As per Avogadro's law, the flue gas at NTP occupies same volume as air used at NTP

Similarly value of flue gases inside chimney :-

$$\frac{V_g}{T_g} = \frac{V_0}{T_0} \Rightarrow V_g = \frac{0.7732}{273} m_a T_g$$

So,

$$\beta_g = \frac{m_g}{V_g} = \frac{m_a + 1}{V_g} = \frac{m_a + 1}{0.7732 m_a} \times \frac{273}{T_g}$$
$$= \frac{353}{T_g} \left(\frac{m_a + 1}{m_a} \right)$$

So, from eqⁿ (A) (B) & (C)

$$\Delta P = \left[\frac{353}{T_a} - \frac{353}{T_g} \left(\frac{m_a + 1}{m_a} \right) \right] g H$$

$$\Delta P = 353 g H \left[\frac{1}{T_a} - \left(\frac{m_a + 1}{m_a} \right) \frac{1}{T_g} \right] \quad \text{N/m}^2$$

In terms of water column (mm of H₂O column)

$$\Delta P = (\rho g h)_w \quad \text{where } \rho_w = 1000 \text{ kg/m}^3$$

$$h_w = h \text{ (mm of water)} = \frac{h}{1000} \text{ meter}$$

⇒

$$\Delta P = 1000 \text{ kg/m}^3 \times g \times \frac{h}{1000} \text{ m}$$

$$\Delta P \Rightarrow 1000 g h \quad \frac{\text{kg/m}^2}{\text{m}} \quad (5)$$

So from eqⁿ (D) & (5)

we have

$$\cancel{1000} g h =$$

$$g h = 353 g H \left[\frac{1}{T_a} - \left(\frac{m_a + 1}{m_a} \right) \frac{1}{T_g} \right]$$

$$h = 353 H \left[\frac{1}{T_a} - \left(\frac{m_a + 1}{m_a} \right) \frac{1}{T_g} \right]$$

Now assuming draught ΔP produced is equivalent to H_1 meters of burnt gases, we have

$$\Delta P = \rho_g g H_1 = 353 \left(\frac{m_a + 1}{m_a} \right) \frac{1}{T_g} g H_1 \quad (6)$$

From eqⁿ (D) & (6)

$$\cancel{353} \left(\frac{m_a + 1}{m_a} \right) H_1 \cancel{g} \frac{1}{T_g} = \cancel{353} \cancel{g} H \left[\frac{1}{T_a} - \left(\frac{m_a + 1}{m_a} \right) \frac{1}{T_g} \right]$$

$$\Rightarrow H_1 = H \left(\frac{m_a}{m_a + 1} \right) T_g \left[\frac{1}{T_a} - \left(\frac{m_a + 1}{m_a} \right) \frac{1}{T_g} \right]$$

$$H_1 = H \left[\left(\frac{m_a}{m_a + 1} \right) \frac{T_g}{T_a} - 1 \right]$$

Now

Diameter of chimney :

\therefore The theoretical velocity of hot flue gases flows through chimney

$$C_g = \sqrt{2gH_1}$$

Consider h_f = frictional losses in column of hot flue gases
then

$$C_g = \sqrt{2g(H_1 - h_f)}$$

$$C_g = 4.43 \sqrt{H_1 - h_f} \Rightarrow C_g = 4.43 \sqrt{H_1} \times \sqrt{1 - \frac{h_f}{H_1}}$$

$$C_g = 4.43 \sqrt{H_1} \times \sqrt{1 - \frac{h_f}{H_1}}$$

$$C_g = k \sqrt{H_1} \quad \text{where, } k = 4.43 \sqrt{1 - \frac{h_f}{H_1}}$$

Experimentally -
 $k = 0.825$ for brick chimney
 $= 1.1$ (steel chimney)

Mass of flue gases flowing through chimney

$$\dot{m}_g = \rho_g A C_g \quad (\text{kg/s})$$

$$= \rho_g \left(\frac{\pi D^2}{4} \right) C_g$$

$$D^2 = \frac{4 \dot{m}_g}{\pi \rho_g C_g}$$

$$D = 1.128 \sqrt{\frac{\dot{m}_g}{\rho_g C_g}}$$

Condition for maximum discharge through chimney

$$C_g = \sqrt{2gH_1} \quad \text{where } h_f = 0$$

$$C_g = \sqrt{2gH_1 \left[\left(\frac{m_g}{m_a + 1} \right) \frac{T_g}{T_a} - 1 \right]}$$

$$\dot{m}_g = \rho_g A C_g = A \rho_g \sqrt{2gH_1 \left[\left(\frac{m_g}{m_a + 1} \right) \frac{T_g}{T_a} - 1 \right]}$$

$$= A \left[\sqrt{2gH_1 \left[\left(\frac{m_g}{m_a + 1} \right) \frac{T_g}{T_a} - 1 \right]} \right] \left[\frac{P}{RT_g} \right]$$

For maximum discharge $\frac{d\dot{m}_g}{dT_g} = 0$

Final result

$$\frac{T_g}{T_a} = 2 \frac{m_a + 1}{m_a}$$

$$\Rightarrow (H_1)_{\max} = H \quad \left| \quad (hw)_{\max} = \frac{176.5}{T_a} H \text{ mm of water} \right.$$